COMDTPUB P16700.4 **NVIC 11-91** 16 Jul 1991

NAVIGATION AND VESSEL INSPECTION CIRCULAR NO. 11-91

Subj: Ocean Tow of Jackup Drilling Units

- 1. <u>PURPOSE</u>. The purpose of this Circular is to call attention to and endorse the International Association of Drilling Contractors (IADC) booklet entitled "General Ocean Tow Recommendations for Jackup Drilling Units" dated February 13, 1991.
- 2. <u>BACKGROUND</u>. The recent loss of a number of jackup drilling units while under tow in severe storms emphasized to the Coast Guard and industry the need to develop a set of guidelines on the ocean tow of jackup drilling units. The Coast Guard suggested to industry under the auspices of the National Offshore Safety Advisory Committee (NOSAC) that a working group be formed to study the problem and develop a set of guidelines. This working group consisted of personnel from the drilling industry, classification societies and insurance underwriters marine surveyors. The guideline booklet was completed and accepted by NOSAC at its February 21, 1991 meeting, with the request that it be issued by the Coast Guard as a Navigation and Vessel Inspection Circular.
- 3. DISCUSSION. The Coast Guard endorses the quidelines set out in enclosure (1). Use of these quidelines by drilling contractors, classification society surveyors and insurance underwriters marine surveyors will reduce the risk of the loss of jackup drilling units during severe storms while under ocean tow.

4 **IMPLEMENTATION**.

- Officers in Charge, Marine Inspection are urged to bring enclosure (1) to the attention of a. appropriate individuals in the offshore industry in their zones.
- b. Owners, classification societies and marine under writers should implement the recommendations of enclosure (1) in order to reduce the risk of the loss of jackup units.

E. HENN

Rear Admiral, U.S. Coast Guard Chief, Office of Marine Safety,

Security and Environmental Protection

End: (1) General Ocean Tow Recommendations for Jackup Drilling Units (IADC) dated February 13, 1991

GENERAL OCEAN TOW RECOMMENDATIONS FOR JACKUP DRILLING UNITS International Association of Drilling Contractors (I.A.D.C.)

February 13, 1991

Manning

1. Manning should comply with U.S. Coast Guard regulations or other national regulatory rules. The number of crew will be dependent on the length of the voyage and be limited to essential personnel only and should not exceed 50 % of lifeboat capacity.

Ocean Tow Loading Plan

- 2. A Loading Plan should be formulated and, if required, submitted to the Underwriter's Marine Survey company utilized by the Contractor for the tow in time for proper review. (See Addendum A enclosed for a sample loading plan)
- 3. Cargo is defined as any material, temporary structure, shipping container, consumable item, machinery, tubular, equipment and items not included in the drill barge lightship weight.
- 4. Stowage of on the main weather deck of a Jackup drilling unit while on an ocean tow is not desirable and should be avoided with the exceptions noted below.
- 5. Exceptions to this policy my be permitted if:
 - a. A permanent structure has been erected for the stowing and securing of an item such as a pipe rack for drill pipe and drill collars, or a mandrel and locking beams for a BOP. The permanent structures should be adequate for their intended purpose, reviewed, and approved by a classification society in accordance with the appropriate rules.
 - b. Cargo is elevated or located above the main deck by mans of a suitable support structure.
 - c. Temporary structures are permitted when designed by a registered professional engineer and approved by the underwriter's marine surveyor.

<u>Towage</u>

- 6. One set of up-to-date navigation charts and pilot books for the tow course and alternate courses should be available for the voyage aboard the rig including detailed charts of ports of refuge.
- 7. Tow routing should be determined in advance including ports of refuge and the required entry data.
- 8. A weather service should be selected with a beck ground in ocean tow forecasting. Weather updates should be sent every 12 hours with at least 72 hour advance forecasts. Direct communication with a marine weather forecaster is recommended.
- 9. The Towing vessel(s), and towing gear, should be designed and equipped for towing in ocean service with full crew aboard. Towing gear should be inspected and approved by the attending marine and the O.I.M. prior to departure.
- 10. The bollard pull of the towing vessel(s) should be of sufficient size for the intended tow.
- 11. Communication means between the rig and the towing vessel(s) is of utmost importance. Backup communications should be provided. The vessel should provide a qualified riding crew member to assist the rig crew during tow. Language should not be a barrier.

- 12. Critical motion curves should be provided to the rig crew and the towing vessel(s) prior to departure. (see addendum B) Manufacture recommendations for proper leg length and shimming should be adhered to for the tow.
- 13. An emergency towing line should be strapped along the side of the hull just below top deck level in a manner permitting quick release. me tow line should be of a size suitable for the tow intended accounting for the bollard pull of the tow vessel(s), including shock loads.
- 14. A polypropylene shock line, the size and length suitable for the bollard pull of the tow vessel(s) being used, should be attached to the emergency tow line with suitable connectors.
- 15. A main tow line bridle recovery line(s) should be fitted and run from the and of the bridle or tow plate to a winch on the barge to allow retrieval in the main tow wire(s) part.

Stability

16. stability calculations addressing the tow conditions should be performed to insure positive stability in compliance with the rig operating manual. These calculations should be submitted to and approved by the underwriter's Marine Survey company being utilized in time for proper review. (see Addendum A)

Draft and Trim

- 17. Within the limits of the loadline certificate, the man draft for the tow should be determined from the stability calculations in item 16 above.
- 18. Weight should be distributed to produce a level condition transversely with a slight trim by the stern. Trim is to be obtained by locating material or equipment carried with necessary liquid trimming ballast kept to a minimum.
- 19. Liquid variable load should be kept to a minimum. Hull tanks that contain liquids should be pressed and maintained full during the voyage.
- 20. All tanks, including active mud tanks, not required on the voyage, should be empty at the time of departure.

Watertight Integrity

- 21. The operating manual for the rig should clearly show the location of watertight closures and should be complied with during the tow.
- 22. Deck openings such as sounding tubes should be protected from damage
- 23. Consideration should be given to the modification all weather deck preload hatch covers, vent fan covers, cargo hatch cover, etc. with clamp bars or welded strapping to prevent opening from sea action.
- 24. Rig service take on lines Such as out, barite, fuel, potable water, or drill water located on the outer lull areas should be capped and protected from sea damage by sea action.
- 25. All weather/watertight closures, ventilation ducts, etc. with the exception of intakes necessary for the operation of the vessel, should be seed from sea action.

Pumping Arrangements

26. The vessel's bilge/ballast service pumps should be tested and determined to be in good working order prior to departure. Pumps are to be maintained in a state of readiness throughout the tow.

Compartment Sounding

- 27. All hull compartments and void spaces should be fitted with sounding tubes. All sounding tubes should be clearly identified and fitted with caps that are capable of being tightly secured.
- 28. Soundings should be taken at least every 12 hours of all void and preload tanks. Hull compartments should be inspected or sounded also and the results should be logged for the duration of the
- 29. A diagram of the sounding tube locations should be posted in the machinery deck spaces and in the control room.
- 30. A means of determining the changes in liquid levels in the perimeter hull tanks must be available for use from a protected location.
- 31. The manufacturer's data should be furnished to indicate that the derrick can withstand the roll motions anticipated for the tow. This data should be in the rig operating manual.
- 32. All Derrick traveling equipment should be seared for the tow.
- 33. Bow_anchors should be removed from below water racks and strapped to the deck or stored if there is the possibility of becoming entangled in the tow gear.
- 34. Secure or remove anchor buoys from their racks to prevent dislodging by sea action.

<u>Cranes</u>

- 35. Crane should be lowered into steel support structures and secured against vertical or lateral movement.
- 36. Cranes should be secured against revolving per manufactures recommendations.

Navigation Lights, Signals and Safety Equipment

- 37. Side Lights and stern light should be checked to make sure they are in good working order.
- 38. Life vests, throw over life rings and other means of rescue should be checked and readied for deployment, if need.
- 39. Signaling devices should be stored in the control room, inspected and determined that they are within inspection dates for use, if needed.

Potable Water and Fuel Oil

40. Sufficient potable water and fuel for the length of the tow, plus 25% safety factor, should be carried.

- 41. A potable pump should be available to obtain water from the potable water tanks in the event of pump failure.
- 42. Because sediment in the fuel tanks can be stirred up during tow, a centrifuge should be installed prior to departure to remove contaminants from the fuel pumped to the engine day tanks. Extra engine fuel filters should be in supply.

Damage Control

43. The following emergency and/or damage control equipment and material is recommended to carried aboard for the tow, or it's equivalent.

400 lbs. cement 400 lbs. sad 20 lbs. concrete mix accelerator 40 ft. of 1" x 12" timber 24 lbs. of oakum or similar caulking compound 24 wooden wedges 24 wooden plugs of various sizes Welding and cutting apparatus 50 ft. of 4" x 4" angle iron 100 sq. ft. of 1/2" steel plate. 100 sq. ft. of 1" steel plate 500 ft. 1" polypropylene rope 500 ft. 1" wire rope 20 Ton Portapower hydraulic jack 100 ft. 2" x 4" x 10' timber Two portable diaphragm air pumps

- 44. Spare shackle, heaving lines, turnbuckles, etc. should be aboard for the tow.
- 45. Fog horn, ship whistle or bell, search light, etc. should be in operating condition.
- 46. Secure all equipment in the accommodations area for heavy seas.
- 47. Strip water from the preload tanks, unused drill water tanks and void tanks prior to and during the tow.
- 48. Lifeboat machinery and equipment should be checked for compliance with existing regulations and be in proper operating condition. Lifeboat fuel tanks should be checked for contaminants and feel cleaned or replaced as necessary Spare fuel filters should be stowed aboard the lifeboat for use, if required.
- 49. The emergency power source should be available for use at all times and teed at periodic intervals

Riding Crew Instructions

- 50. Sea watches should be maintained at all times during the tow. The following information should be entered into the log:
 - a. Weather data including; wind force, wave/swell height/Period.

- b. Motion characteristics of the vessel are of the utmost importance. The Drill Barge Master (licensed or unlicensed) must observe degrees of pitch and roll and their corresponding periods and request the tug to change course and/or speed to prevent the Drill Barge motions from exceeding the values given in the Operations Manual critical motion curves.
- c. All important communication with the towing vessel(s) including speed, course, change in tow wire length, etc. should be recorded.
- d. me Position should be obtained from the towing vessel(s) every 6 hours and recorded in the rig log.
- 51. Each hull tank should be sounded and logged every 12 hours.
- 52. All watertight doors between compartment and from the compartments to outside exits should be kept closed at all times except when personnel pass.
- 53. Tow gear should be inspected every 6 hours and the results logged.
- 54. At least two (2) members of the crew should be awake at all times.
- 55. Radio contact mist be maintained on a 24 hour basis with the tow vessel(s).
- 56. Emergency drills should be held prior to departure and once a week during the tow. Results should be logged.
- 57. All navigation lights should be checked every 6 hours and the results logged.
- 58. Daily reports are should be forwarded to the Contractor's headquarters at least daily.

OCEAN TOW LOADING PLAN ADDENDUM A

FEBRUARY 13, 1991

ADDENDUM A

TO: General Marine Surveyor Company

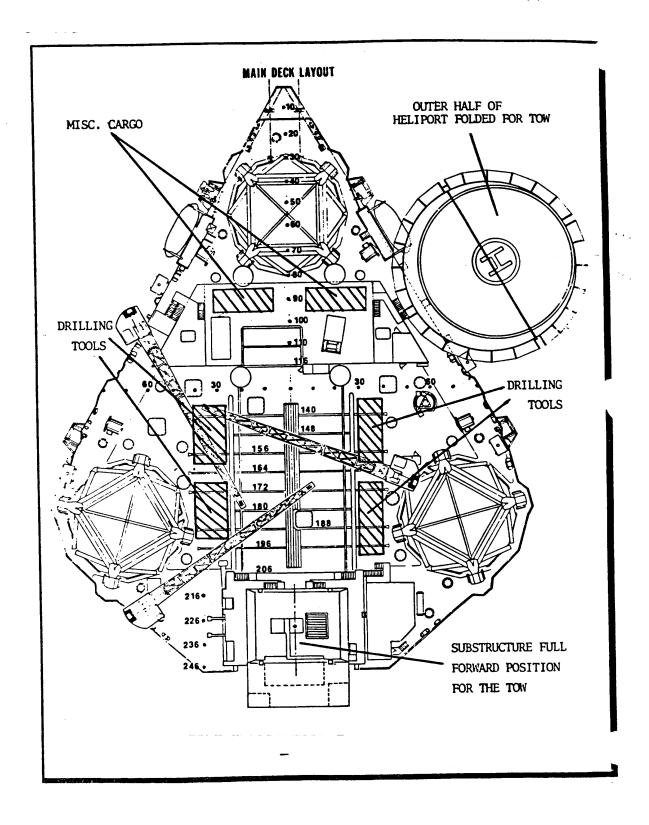
FROM: United Marine Drilling Contractors

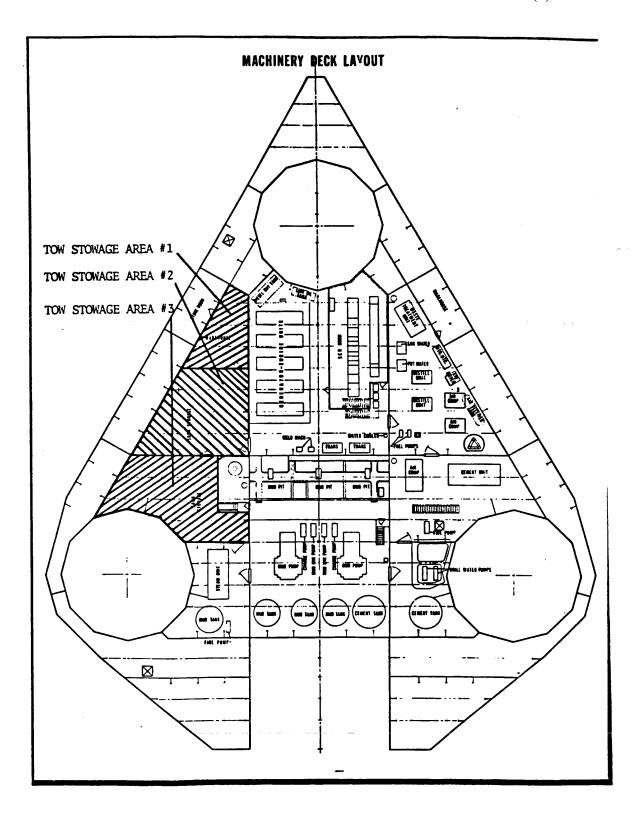
SUBJ: Ocean Tow Stowage Plan

Please review the enclosed Ocean Tow Loading Plan for our 116 class hull. The loading plan is comprised of the following:

- 1. A completed loading calculation for the start of the tow based on the latest information from our rig survey. The stability calculations are based on two leg down positions (12.17 ft. for 70 knots and 45.90 ft. for severe storm).
- 2. All loose gear will be stowed below deck in stowage areas 11 through 13 and secured to prevent shifting during the tow. (see enclosed drawings)
- 3. The drilling tubulars will be secured with turnbuckles and chain and containment barriers will be fabricated at the ends of the racks, subject to your final approval. Four areas are anticipated at this time. (see enclosed drawings)
- 4. Two miscellaneous cargo areas will be constructed on top of the quarters in containment areas in order to remove these items from possible sea action. (see enclosed drawings)
- 5. The Substructure/drill floor assembly will be in the full forward position for the tow and secured to the hull with the clamping arrangement provided by the manufacturer.
- 6. The emergency tow gear will be strapped along the port side of the hull and provisions made for the deployment in severe weather if the need should arise.
- 7. The deepwell tower will be secured to the hull with clamping arrangements designed by the manufacturer. Three 3/4 inch guy wires will be connected to the tower in three different directions securing the tower from the rig motions anticipated.

Please review the Loading Plan provided at this time. As you kn ow, final loading will depend on your survey prior to the departure of the rig.





							DATE:	NOV 1,1990		
	CALCULATIONS FOR: 00	EAN TOW					SHEET NO.	1 OF 4		
EM	DESCRIPTION HT's	WEIGHT	LEVER	FROM BOW	LEVER	STBD-PORT	LEVER	FROM KEEL	TFSC	LFSC
n.	PORT INS.	(IN KIPS)	LCG	(FT. KIPS)	TCG	(FT. KIPS)	VCG	(FT. KIPS)		
==: 8	POTABLE WATER TANK #1 72	308.390	100.17	30,891.423	13.00	4,009.070	3.00	925.170	0.0000	0.0000
9	DRILL WATER TANK #3 0	0.000	100.94	0.000	36.71	0.000	0.00	0.000	0.0000	0.0000
0		231.290	128.17	29,644.438	13.00	3,006.770	3.00	693.870	0.0000	0.000
1	DRILL WATER TANK #7 20	87.028	129.30	11,252.689	45.27	3,939,747	0.83	72.523	0.3275	0.135
	DRILL WATER TANK #15 20	71.161	193.29	13,754,729	13.00	925.094	0.83	59.301	0.1264	0.139
	DRILL WATER TANK #21 0	0.000	0.00	0.000	0.000	0.000	0.00	0.000	0.0000	0.000
4	D/WATER,D/FUEL,BRINE #9 0	0.000	168.08	0.000	13.00	0.000	0.00	0.000	0.0000	0.000
5	DIESEL FUEL TANK #11 72	266.240	156.13	41,568.042	38.97	10,375.371	3.00	798.720	0.0000	0.000
	DIESEL FUEL TANK #13 72	174.200	152.59	26,581.173	63.53	11,066.924	3.00	522.600	0.0000	0.000
7	DIESEL FUEL TANK #17 72	271.170	190.47	51,649.750	38.53	10,448.180	3.00	813.510	0.0000	0.000
	DIRTY OIL TANK #35 0	0.000	121.17	0.000	28.00	0.000	0.00	0.000	0.0000	0.000
9	PORT MUD PIT 0 0	0.000	148.17	0.000	17.87	0.000	6.00	0.000	0.0000	0.000
20	CENTER MUD PIT 0 0	0.000	147.54	0.000	0.87	0.000	6.00	0.000	0.0000	0.000
		0.000	153.18	0.000	6.93	0.000	6.00	0.000	0.0000	0.000
1		0.000	199.58	0.000	41.21	0.000	0.00	0.000		
3	BULK TANK #2 (1040 CU.FT.)	0.000	197.83	0.000	20.00	0.000	0.00	0.000		
-		0.000	197.83	0.000	6.00	0.000	0.00	0.000		
4	BULK TANK #3 (1040 CU.FT.)	20.000	100.00	2,000.000	0.00	0.000	35.00	700.000		
5	CREW & EFFECTS	5.000	85.35	426.750	45.15	225.750	8.00	40,000		
6			94.44	3,777.600	34.82	1,392.800	8.00	320.000		
7	WAREHOUSE (STOWAGE #1)	40.000		18,840.000	43.89	6,583.500	8.00	1,200.000		
28	SACK ROOM (STOWAGE #2)	150.000	125.60	40,214.200	48.89	12,711.400	8.00	2,080.000		
29	HOPPER ROOM (STOWAGE #3)	260.000	154.67	0.000	0.00	0.000	0.00	0.000		
50	ENGINE ROOM	0.000	0.00		34.90	4,135.650	29.50	3,495.750		
31	DRILL PIPE RACK #1	118.500	153.30	18,166.050	34.90	2,024.200	28.00	1,624.000		
32	DRILL PIPE RACK #2	58.000	185.30	10,747.400	48.00	1,209.600	28.00	705.600		
33	HYDRILL	25.200	209.00	5,266.800	0.00	0.000	0.00	0.000		
54	CASING	0.000	0.00	0.000		300.000	54.00	810.000		
55	MISC. (QUARTERS TOP)	15.000	90.00	1,350.000	20.00	0.000	0.00	0.000		
36		0.000	0.00	0.000	0.00	1,886.000	40.00	1,840.000		
57	PORT LEG AREA	46.000	200.00	9,200.000	41.00	•	28.00	140.000		
38	DRUMS ON BOW GEAR UNIT, UPPER	5.000	74.00	370.000	0.00	0.000	28.00	3,480.400		
39	28 JTS 8" D.C.	124.300	150.17	18,666.131	40.00	4,972.000		0.000		
40		0.000	0.00	0.000	40.00	0.000	0.00			
41		0.000	0.00	0.000	37.00	0.000	0.00	0.000		
42		0.000	0.00	0.000	29.00	0.000	0.00	0.000		
43		0.000	0.00	0.000	0.00	0.000	0.00	0.000		
44		0.000	0.00	0.000	0.00	0.000	0.00	0.000		
45		0.000	0.00	0.000	0.00	0.000	0.00	0.000		
46		0.000	0.00	0.000	0.00	0.000	0.00	0.000		
47		0.000	0.00	0.000	0.00	0.000	0.00	0.000		
48		0.000	0.00	0.000	0.00	0.000	0.00	0.000		
49		0.000	0.00	_ 0.000	0.00	0.000	0.00	0.000		
50		0.000	0.00	0.000	0.00	0.000	0.00	0.000		
51		0.000	0.00	0.000	0.00	0.000	0.00	0.000		
	SUB TOTAL-PORT	2,276.479	146.88	334,367.176	-34.80	(79,212.055	8.93	20,321.444	0.4539	0.27

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	CALCULATIONS FOR:	DCEAN TOW					SHEET NO.	2 OF 4		
ITEM	DESCRIPTION HT's	WEIGHT	LEVER	FROM BOW	LEVER	STBD-PORT	LEVER	FROM KEEL	TFSC	LFSC
NO.		(IN KIPS)	LCG	(FT. KIPS)	TCG	(FT. KIPS)	VCG	(FT. KIPS)		
61	POTABLE WATER TANK #2 50	214.160	100.17	21,452.377	13.00	2,784.076	2.08	446.166		
62		182.667	100.94	18,438.372	36.71	6,705.693	2.08	380.556	0.1130	0.2697
63	DRILL WATER TANK #6 0	0.000	128.17	0.000	13.00	0.000	0.00	0.000	0.0000	0.0000
64		0.000	128.63	0.000	43.71	0.000	0.00	0.000	0.0000	0.0000
65	DRILL WATER TANK #16 50	177.903	193.29	34,386.823	13.00	2,312.736	2.08	370.631	0.1264	0.1398
	D/WATER,D/FUEL,BRINE #10 0	0.000	168.08	0.000	13.00	0.000	0.00	0.000	0.0000	0.0000
67		252,050	156.45	39,433.217	39.33	9,913.125	3.00	756.150	0.0000	0.0000
68	DIESEL FUEL TANK #14 72	174.200	152.59	26,581.173	63.53	11,066.924	3.00	522.600	0.0000	0.0000
69	DIESEL FUEL TANK #20 0	0.000	197.81	0.000	38.33	0.000	0.00	0.000	0.0000	0.0000
70	STARBOARD MUD PIT 0 0	0.000	148.17	0.000	17.87	0.000	0.00	0.000	0.0000	0.0000
71	MUD PIT SAND TRAP 0	0.000	148.17	0.000	23.25	0.000	0.00	0.000		
72	BULK TANK #4 (1040 CU.FT.)	0.000	197.83	0.000	6.00	0.000	6.50	0.000		
73	BULK TANK #5 (1323 CU.FT.)	0.000	197.83	0.000	18.50	0.000	6.50	0.000		
74	BULK TANK #6 (1323 CU.FT.)	0.000	197.83	0.000	38.96	0.000	6.50	0.000		
75	AIR COMPRESSOR ROOM	3.000	118.00	354.000	38.00	114.000	9.00	27.000		
76	MECHANIC SHOP	5.000	85.35	426.750	45.15	225.750	12.00	60.000		
77	POLLUTION CONTROL TANK	0.000	210.00	0.000	62.00	0.000	0.00	0.000		
78	CEMENT UNIT ROOM	3.000	153.00	459.000	58.00	174.000	8.00	24.000		
79	PUMP ROOM	3.000	182.00	546.000	0.00	0.000	8.00	24.000		
80	DRILL PIPE RACK #1	118.500	142.90	16,933.650	34.70	4,111.950	28.00	3,318.000		
81	DRILL PIPE RACK #2	258.000	184.90	47,704.200	34.70	8,952.600	29.50	7,611.000		
82	PAINT LOCKER & CONTENTS	6.000	62.00	372.000	29.00	174.000	29.00	174.000		
83	MUD LOG HOUSE	0.000	220.00	0.000	38.00	0.000	48.00	0.000		
84	ELECTRIC WIRE LINE UNIT	0.000	105.00	0.000	20.00	0.000	0.00	0.000		
85	SAND TRAPS	0.000	229.00	0.000	38.00	0.000	0.00	0.000		
86	CASING	0.000	0.00	0.000	0.00	0.000	0.00	0.000		
87	HELI. FUEL	15.580	90.00	1,402.200	10.85	169.043	56.00	872.480		
88	OXY/ACET. RACKS	7.000	144.00	1,008.000	40.00	280.000	28.00	196.000		
89	MISC. (QUARTERS-TOP)	12.000	90.00	1,080.000	20.00	240.000	54.00	- 648.000		
90	•	0.000	0.00	0.000	0.00	0.000	0.00	0.000		
91		0.000	0.00	0.000	0.00	0.000	0.00	0.000		
92		0.000	0.00	0.000	0.00	0.000	0.00	0.000		
93		0.000	0.00	0.000	0.00	0.000	0.00	0.000		
94		0.000	0.00	0.000	0.00	0.000	0.00	0.000		
95		0.000	0.00	0.000	0.00	0.000	0.00 0.00	0.000		
96		0.000	0.00	0.000		0.000	0.00	0.000		
97		0.000	0.00		0.00					
98		0.000	0.00	0.000	0.00	0.000	0.00 0.00	0.000		
99		0.000	0.00 0.00	0.000	0.00	0.000	0.00	0.000		-
100		0.000	0.00	0.000	0.00	0.000	0.00	0.000		
101		0.000	0.00	0.000	0.00	0.000	0.00	0.000		
102		0.000	0.00	0.000	0.00	0.000	0.00	0.000		
103	CUR-TOTALCTARROARD	1,432.059	147.05	210,577.762	32.98	47,223.897	10.78	15,430.582	0.3016	0.6422
104	SUB-TOTALSTARBOARD	3,708.538	146.94	544,944.938		(31,988.158)		35,752.026		
105	TOTAL PORT & STBD.	3,100.330	140.74	J44,744.730	-0.03	(31,700.130)	7.07	33,136.020	7.0433	3.7174

	***************************************							DATE: N	IOV 1,1990		
	CALCULATIONS FOR:	00	CEAN TOW					SHEET NO.	3 OF 4		
TEM	DESCRIPTION	HT's	WEIGHT	LEVER	FROM BOW	LEVER	STBD-PORT	LEVER	FROM KEEL	TFSC	LFSC
•	LOADING CIMMADY	INS.	(IN KIPS)	LCG	(FT. KIPS)	TCG	(FT. KIPS)	VCG	(FT. KIPS)		
	FERENCESSESSESSESSESSESSESSESSESSESSESSESSESS				***********		25522222222	20222222			
				440.50	45.11.1 50011400	00017100	1/0 ER ET \				
	ENTER POSTION OF ROTORY F	ROM B	OM 3	149.58	(FULL FORWARD	POSTITUM	149.30 F1.)				
	SUBBASE LOADING				0 00/ 000	-15 00	(825.000)	32 00	1,760.000		
	B.O.P. STACK		55.000	149.58	8,226.900 0.000	20.00	0.000	0.00	0.000		
17			0.000	0.00	2.016.840	7.32	87.840	32.00	384.000		-
	PARTS FOR DIVERTER SYS		12.000	168.07	0.000	0.00	0.000	0.00	0.000		
	CHANGES TO SUBBASE ASSY.		0.000	0.00		-1.83	(264.691)		4,683.443		
	SUBBASE ASSY.		144.640	153.07	22,140.045	-4.73	(1,001.851)		6,827.443		
21	TOTAL SUBBASE ASSY.		211.640	153.01	32,383.785	-4./3	(1,001.051)				
23	ENTER POSITION OF ROTARY	FROM	C/L)	0.00	(- PORT + STB	D)					
	RIG FLOOR LOADING										
25	HOOK, ROTARY & SETBACK		0.000	149.58	0.000	0.00	0.000	0.00	0.000		
	CONDUCTOR TENSION		0.000	149.58	0.000	0.00	0.000	0.00	0.000		
27	• • • • • • • • • • • • • • • • • • • •		15.000	153.07	2,296.050	0.00	0.000	48.00	720.000		
28	.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		0.000	0.00	0.000	0.00	0.000	0.00	0.000		
29			0.000	0.00	0.000	0.00	0.000	0.00	0.000		
30	CHANGES TO SUB./STR, D.F.		77.800	154.14	11,992.092	0.68	52.904		9,441.808		
31	SUB./STR. &-DRILL FLOOR		786.570	153.07	120,400.270	-1.83	(1,439.423)	61.46	48,342.592		
	TOTAL RIG FLOOR LOADING		879.370	153.16	134,688.412	-1.58	(1,386.519)		58,504.400		
134	TOTAL SUBSTRUCTURE ASSY.		1,091.010	153.14	167,072.197	-2.19	(2,388.370)	59.88	65,331.843		
	TUTAL SUBSTRUCTURE ASST.		9,314.900	477 57	1,281,078.197	3.80	35.396.620	23.80	221,694.620		
	HULL, BASIC & FIXED LOADS		100.760	136.05	13,708.700	9.95	1,002.670	28.79	2,900.650		
	CHANGES TO HULL, BASIC, FIX	KED			1,294,786.897	3.87	36,399.290	23.85	224,595.270		
138	TOTAL HULL, BASIC & FIXED		9,415.660								
140	TOTAL OF ITEMS No.										
	40E 47/ 470 40/		14,215.208	141.17	2,006,804.032	0.14	2,022.761	22.91	325,679.139		
	105,134,136,164	====			809,545.851		2,062.537	134.24	769,097.205		
	LEGS, T.O.C. DOWN 12.17		5,729.270	141.30	2,816,349.883	0.10	4,085.299	54.89	1.094.776.344	0.8455	0.91
144	FIELD TRANSIT (W/ TRIM/H	EEL)	19,944.476	141.21	2,010,347.003	0.10	4,0051277	21107	,,,		
145											
	TRANSFER TO TRIM			00.75	2,770.500	-49.71	(1,491.300)	-4 16	(124.800))	
	TANK #4 TO #15		30.000	92.35	1,477.600		(379.360)		(60.000)		
148			16.000	92.35	0.000		0.000	0.00	0.000		
149			0.000	0.00	0.000		0.000	0.00	0.000		
150			0.000	0.00			0.000	0.00	0.000		
151			0.000	0.00	0.000		2,214.639	54.88	1,094,591.544	0.8455	0.91
	FIELD TRANSIT (LEVEL)		19,944.478	141.42	2,820,597.983	0.11	2,214.037	J4.00	,,0,4,5,,,,		
153								-33.73	(193.248.277))	
	LOWER LEGS (T.O.C. 45.90	')	/		2 820 507 007	0.44	2,214.639	45.19	901,343.267		0.91
	TRANSIT - SEVERE STORM		19,944.478	141.42	2,820,597.983	0.11	2,214.039	77.17	,01,343.201		
156											
157											
158											

	CALCULATIONS FO	R:	c	DCEAN TOW					SHEET N	NOV 1,1990 IO. 4 OF 4		
TEM	DESCRIPTON		HT's	WEIGHT	LEVER	FROM BOW	LEVER	STBD-PORT	· LEVER	FROM KEEL	TFSC	LFSC
Ю.	PRELOAD		In's		LCG	(FT. KIPS)	TCG	(FT. KIPS)	VCG	(FT. KIPS)		
	PRELOAD TK #21		0	0.000	VAR.	0.000	0.000	0.000	0.00		0.0000	0.0000
70	PRELOAD TK #22	(312")	0	0.000	63.27	0.000	28.70	0.000	0.00	0.000	0.0000	0.0000
71	PRELOAD TK #23	(312")	0	0.000	63.33	0.000	-28.58	0.000	0.00	0.000	0.0000	0.0000
72	PRELOAD TK #24	(312")	0	0.000	117.08	0.000	63.47	0.000	0.00	0.000	0.0000	0.0000
73	PRELOAD TK #25	(312")	0	0.000	117.08	0.000	-63.47	0.000	0.00	0.000	0.0000	0.000
74	PRELOAD TK #26	(312")	0	0.000	158.05	0.000	86.24	0.000	0.00	0.000	0.0000	0.000
75	PRELOAD TK #27	(312")	0	0.000	158.05	0.000	-86.24	0.000	0.00	0.000	0.0000	0.000
76	PRELOAD TK #28	(312")	0	0.000	VAR.	0.000	VAR.	0.000	0.00	0.000	0.0000	0.000
77	PRELOAD TK #29	(312")	0	0.000	VAR.	0.000	VAR.	0.000	0.00	0.000	0.0000	0.000
	PRELOAD TK #30		0	0.000	VAR.	0.000	VAR.	0.000	0.00	0.000	0.0000	0.000
79	PRELOAD TK #31		0	0.000	VAR.	0.000	VAR.	0.000	0.00	0.000	0.0000	0.000
80	ALL MUD PITS	(120")	ō	0.000	144.92	0.000	0.61	0.000	6.00		0.0000	0.000
81		(,	•	*****		*****	*					
82												
83												
84	TOTAL PRELOAD			0.000	0.00	0.000	0.00	0.000	0.00		0.0000	
85	TOTAL LOADING (I			19,944.478		2,820,597.983	0.11	2,214.639	54.88	1,094,591.544		
											EEEEEE.	
o/	REALLIUN AFF LE	GS	TOTAL	L LOADING (I	N KIPS) X	((RIG L.C.G.(-)	55.001/	129.001		13.361.64	AFT RE	ACTION
	REACTION AFT LE					((RIG L.C.G.(-) ON ON AFT LEGS	55.00'/	129.001		13,361.64 6.582.84		
88	REACTION BOW LE	G	TOTAL	L LOADING (-) REACTIO	ON ON AFT LEGS				6,582.84	BOW RE	ACTION
	REACTION BOW LE REACTION STBD LE REACTION PORT LE	G G G	REAC	L LOADING (- TION ON AFT TION OF AFT) REACTIC LEGS X (7 (-) PORT	ON ON AFT LEGS 71.00' (+) RIG T OR STBD LEG REA	.C.G.) /	142.00'		6,582.84 6,691.27 6,670.37	BOW RESTED REPORT RE	ACTION ACTION ACTION
88 89 90	REACTION BOW LE REACTION STBD LE REACTION PORT LE	G G G	REAC	L LOADING (- TION ON AFT TION OF AFT) REACTIC LEGS X (7 (-) PORT	ON ON AFT LEGS 71.00' (+) RIG T OR STBD LEG REA	.C.G.) /	142.00'		6,582.84 6,691.27 6,670.37	BOW RESTED REPORT RE	ACTION ACTION ACTION
88 89 90	REACTION BOW LE REACTION STBD LE REACTION PORT LE TOTAL CALCULATED	G G G LOAD	TOTAI REAC REAC	L LOADING (- TION ON AFT TION OF AFT) REACTIC LEGS X (7 (-) PORT	ON ON AFT LEGS 71.00' (+) RIG T OR STBD LEG REA VARIABLE LOAD-	.C.G.) / CTION STORM	142.00° 4,053.890	KIPS	6,582.84 6,691.27 6,670.37 	BOW RE STBD RE PORT RE	ACTION ACTION ACTION
88 89 90 92 93	REACTION BOW LE REACTION STBD LE REACTION PORT LE TOTAL CALCULATED LESS HOOK, ROTORY	G G G LOAD	TOTAI REAC REAC	L LOADING (- TION ON AFT TION OF AFT) REACTIC LEGS X (7 (-) PORT	ON ON AFT LEGS 71.00' (+) RIG T OR STBD LEG REA VARIABLE LOAD- VARIABLE LOAD-	.C.G.) / CTION STORM	142.00° 4,053.890 (3,969.098)	KIPS KIPS	6,582.84 6,691.27 6,670.37 ANGLE OBSERVED TRIM	BOW RE STBD RE PORT RE	ACTION ACTION ACTION DEGRE
88 89 90 92 93 94	REACTION BOW LE REACTION STBD LE REACTION PORT LE TOTAL CALCULATED	G G G LOAD	TOTAI REAC REAC	L LOADING (- TION ON AFT TION OF AFT) REACTIC LEGS X (7 (-) PORT	ON ON AFT LEGS 71.00' (+) RIG T OR STBD LEG REA VARIABLE LOAD-	.C.G.) / CTION STORM	142.00° 4,053.890	KIPS KIPS	6,582.84 6,691.27 6,670.37 	BOW RE STBD RE PORT RE	ACTION ACTION ACTION DEGRE
88 89 90 92 93 94 95	REACTION BOW LE REACTION STBD LE REACTION PORT LE TOTAL CALCULATED LESS HOOK, ROTORY LESS CONDUCTOR 1	G G LOAD & SETBA	TOTAI REAC' REAC'	L LOADING (- TION ON AFT TION OF AFT) REACTIC LEGS X (7 (-) PORT	ON ON AFT LEGS 71.00' (+) RIG T OR STBD LEG REA VARIABLE LOAD- VARIABLE LOAD- MAKE UP PRELOA	C.G.) / CTION STORM MOVE	4,053.890 (3,969.098) 84.792	KIPS KIPS KIPS	6,582.84 6,691.27 6,670.37 ANGLE OBSERVED TRIM	BOW RE STBD RE PORT RE	ACTION ACTION ACTION DEGRE
88 89 90 92 93 94 95 96	REACTION BOW LE REACTION STBD LE REACTION PORT LE TOTAL CALCULATED LESS HOOK, ROTORY LESS CONDUCTOR 1 LESS TOTAL LIGHT	G G LOAD & SETBA	TOTAI REAC' REAC'	L LOADING (- TION ON AFT TION OF AFT) REACTIC LEGS X (7 (-) PORT =======	ON ON AFT LEGS 71.00' (+) RIG T OR STBD LEG REA VARIABLE LOAD- VARIABLE LOAD- MAKE UP PRELOA MINIMUM PRELOA	C.G.) / CTION STORM MOVE	4,053.890 (3,969.098) 84.792 8,650.000	KIPS KIPS KIPS	6,582.84 6,691.27 6,670.37 	BOW RE STBD RE PORT RE 0.10 0.00	ACTION ACTION ACTION DEGRE
88 89 90 92 93 94 95 96 97	REACTION BOW LE REACTION STBD LE REACTION PORT LE TOTAL CALCULATED LESS HOOK, ROTORY LESS CONDUCTOR T LESS TOTAL LIGHT TOTAL VARIABLE	G G G LOAD & SETBA ENSION	TOTAI REAC REAC	L LOADING (- TION ON AFT TION OF AFT) REACTIC LEGS X (7 (-) PORT =======	ON ON AFT LEGS 71.00' (+) RIG T OR STBD LEG REA VARIABLE LOAD- VARIABLE LOAD- MAKE UP PRELOA MINIMUM PRELOA MAKE UP PRELOA	C.G.) / CTION STORM MOVE	4,053.890 (3,969.098) 84.792 8,650.000 84.792	KIPS KIPS KIPS KIPS	6,582.84 6,691.27 6,670.37 ANGLE OBSERVED TRIM HEEL	BOW RE STBD RE PORT RE 0.10 0.00	ACTION ACTION ACTION DEGRE DEGRE
88 89 90 92 93 94 95 96 97 98	REACTION BOW LE REACTION STBD LE REACTION PORT LE TOTAL CALCULATEE LESS HOOK, ROTORY LESS CONDUCTOR T LESS TOTAL LIGHT TOTAL VARIABLE MAX. VARIABLE	G G G LOAD & SETBA ENSION SHIP	TOTAI REAC REAC REAC RCK	L LOADING (- TION ON AFT TION OF AFT) REACTIC LEGS X (7 (-) PORT =======	ON ON AFT LEGS 71.00' (+) RIG T OR STBD LEG REA VARIABLE LOAD- VARIABLE LOAD- MAKE UP PRELOA MINIMUM PRELOA	C.G.) / CTION STORM MOVE	4,053.890 (3,969.098) 84.792 8,650.000	KIPS KIPS KIPS KIPS	6,582.84 6,691.27 6,670.37 	BOW RE STBD RE PORT RE 0.10 0.00	ACTION ACTION ACTION DEGRE DEGRE
88 89 90 92 93 94 95 96 97 98 99	REACTION BOW LE REACTION STBD LE REACTION PORT LE TOTAL CALCULATE LESS HOOK, ROTORY LESS CONDUCTOR 1 LESS TOTAL LIGHT TOTAL VARIABLE MAX. VARIABLE LO MAX. VARIABLE LO	G G G LOAD & SETBA ENSION SHIP DAD (STORAD)	TOTAI REAC REAC REAC REACK	L LOADING (- TION ON AFT TION OF AFT) REACTIC LEGS X (7 (-) PORT =======	ON ON AFT LEGS 71.00' (+) RIG T OR STBD LEG REA VARIABLE LOAD- VARIABLE LOAD- MAKE UP PRELOA MINIMUM PRELOA MAKE UP PRELOA	C.G.) / CTION STORM MOVE	4,053.890 (3,969.098) 84.792 8,650.000 84.792	KIPS KIPS KIPS KIPS	6,582.84 6,691.27 6,670.37 ANGLE OBSERVED TRIM HEEL	BOW RE STBD RE PORT RE 0.10 0.00	ACTION ACTION ACTION CACTION C
88 89 90 92 93 94 95 96 97 98 99 200	REACTION BOW LE REACTION STBD LE REACTION PORT LE TOTAL CALCULATEE LESS HOOK, ROTORY LESS CONDUCTOR T LESS TOTAL LIGHT TOTAL VARIABLE MAX. VARIABLE	G G G LOAD & SETBA ENSION SHIP DAD (STORAD)	TOTAI REAC REAC REAC REACK	L LOADING (- TION ON AFT TION OF AFT) REACTIC LEGS X (7 (-) PORT =======	ON ON AFT LEGS 71.00' (+) RIG T OR STBD LEG REA VARIABLE LOAD- VARIABLE LOAD- MAKE UP PRELOA MINIMUM PRELOA MAKE UP PRELOA	C.G.) / CTION STORM MOVE	4,053.890 (3,969.098) 84.792 8,650.000 84.792	KIPS KIPS KIPS KIPS	6,582.84 6,691.27 6,670.37 ANGLE OBSERVED TRIM HEEL	BOW RE STBD RE PORT RE 0.10 0.00	ACTION ACTION ACTION CACTION C
88 89 90 92 93 94 95 96 97 98 99	REACTION BOW LE REACTION STBD LE REACTION PORT LE TOTAL CALCULATED LESS HOOK, ROTORY LESS TOTAL LIGHT TOTAL VARIABLE MAX. VARIABLE LO MAX. VARIABLE LO MAX. VARIABLE LO	G G G LOAD & SETBA ENSION SHIP DAD (STOR	TOTAL REAC' REAC' ACK RM) LLING)	L LOADING (- TION ON AFT TION OF AFT) REACTIC LEGS X (7 (-) PORT ======= (-)	ON ON AFT LEGS 71.00' (+) RIG T OR STBD LEG REA VARIABLE LOAD- VARIABLE LOAD- MAKE UP PRELOA MINIMUM PRELOA MAKE UP PRELOA MINI REQUIRED	C.C.G.) / ICTION STORM MOVE ID ID ID PRELOAD	142.00° 4,053.890 (3,969.098) 84.792 8,650.000 84.792 8,734.792	KIPS KIPS KIPS KIPS KIPS	6,582.84 6,691.27 6,670.37 ANGLE OBSERVED TRIM HEEL	BOW RE STBD RE PORT RE 0.10 0.00	ACTION ACTION ACTION CACTION C
88 89 90 92 93 94 95 96 97 98 99 200 201	REACTION BOW LE REACTION STBD LE REACTION PORT LE TOTAL CALCULATED LESS HOOK, ROTORY LESS TOTAL LIGHT TOTAL VARIABLE MAX. VARIABLE LO MAX. VARIABLE LO POTABLE WATER TO	G G G LOAD & SETBA ENSION SHIP DAD (STOR DAD (MOVE	TOTAL REAC' REAC' REAC' ACK RM) LING)	L LOADING (- TION ON AFT TION OF AFT) REACTIC LEGS X (7 (-) PORT (-) (+)	ON ON AFT LEGS 71.00' (+) RIG TOOR STED LEG REA VARIABLE LOAD- MAKE UP PRELOA MINIMUM PRELO	C.G.) / ICTION STORM HOVE LD LD PRELOAD	142.00° 4,053.890 (3,969.098) 84.792 8,650.000 84.792 8,734.792	KIPS KIPS KIPS KIPS KIPS KIPS	6,582.84 6,691.27 6,670.37 ANGLE OBSERVED TRIM HEEL	BOW RE STBD RE PORT RE 0.10 0.00	ACTION ACTION ACTION CACTION C
88 89 90 92 93 94 95 96 97 98 99 00 01	REACTION BOW LE REACTION STBD LE REACTION PORT LE TOTAL CALCULATED LESS HOOK, ROTORY LESS CONDUCTOR T LESS TOTAL LIGHT TOTAL VARIABLE MAX. VARIABLE LO MAX. VARIABLE LO POTABLE WATER TO	G G G G G G G G G G G G G G G G G G G	TOTAL REAC'	L LOADING (- TION ON AFT TION OF AFT) REACTIC LEGS X (7 (-) PORT (-) (+)	ON ON AFT LEGS 71.00' (+) RIG T OR STBD LEG REA VARIABLE LOAD- VARIABLE LOAD- MAKE UP PRELOA MINIMUM PRELOA MAKE UP PRELOA MINI REQUIRED	C.G.) / ICTION STORM HOVE LD LD PRELOAD	142.00° 4,053.890 (3,969.098) 84.792 8,650.000 84.792 8,734.792	KIPS KIPS KIPS KIPS KIPS KIPS	6,582.84 6,691.27 6,670.37 ANGLE OBSERVED TRIM HEEL	BOW RE STBD RE PORT RE 0.10 0.00	ACTION ACTION ACTION CACTION C
88 89 90 92 93 94 95 96 97 98 99 00 01 02 03	REACTION BOW LE REACTION STBD LE REACTION PORT LE REACTIO	G G G LOAD & SETBA ENSION SHIP DAD (STOR DAD (MOVE	TOTAL REAC'	L LOADING (- TION ON AFT TION OF AFT) REACTIC LEGS X (7 (-) PORT (-) (+)	ON ON AFT LEGS 71.00' (+) RIG TOOR STED LEG REA VARIABLE LOAD- MAKE UP PRELOA MINIMUM PRELO	C.G.) / ICTION STORM HOVE LD LD PRELOAD	142.00° 4,053.890 (3,969.098) 84.792 8,650.000 84.792 8,734.792	KIPS KIPS KIPS KIPS KIPS KIPS	6,582.84 6,691.27 6,670.37 ANGLE OBSERVED TRIM HEEL	BOW RE STBD RE PORT RE 0.10 0.00	ACTION ACTION ACTION CACTION C
88 89 90 92 93 94 95 96 97 98 99 201 202 203	REACTION BOW LE REACTION STBD LE REACTION PORT LE TOTAL CALCULATED LESS HOOK, ROTORY LESS CONDUCTOR T LESS TOTAL LIGHT TOTAL VARIABLE MAX. VARIABLE LO MAX. VARIABLE LO POTABLE WATER TO	G G G G G G G G G G G G G G G G G G G	TOTAL REAC REAC REAC REAC REAC REAC REAC REAC	L LOADING (- TION ON AFT TION OF AFT) REACTIC LEGS X (7 (-) PORT (-) (+)	ON ON AFT LEGS 71.00' (+) RIG T OR STED LEG REA VARIABLE LOAD- VARIABLE LOAD- MAKE UP PRELOA MINIMUM PRELOA MAKE UP PRELOA MIN. REQUIRED EST REACTION CAL ALLOMABLE LEG R	C.G.) / CTION CTION STORM MOVE D D D CULATED CULATED CULATED	142.00° 4,053.890 (3,969.098) 84.792 8,650.000 84.792 8,734.792	KIPS KIPS KIPS KIPS KIPS KIPS	6,582.84 6,691.27 6,670.37 ANGLE OBSERVED TRIM HEEL	BOW RE STBD RE PORT RE 0.10 0.00	ACTION ACTION ACTION DEGRE DEGRE
88 89 90 92 93 94 95 96 97 98 99	REACTION BOW LE REACTION STBD LE REACTION PORT LE REACTIO	G G G G G G G G G G G G G G G G G G G	TOTAL REAC REAC REACK ACK STATE REACK RM) LING) STATE RS= RS= RS=	L LOADING (- TION ON AFT TION OF AFT) REACTIC LEGS X (7 (-) PORT (-) (+)	ON ON AFT LEGS 71.00' (+) RIG TOOR STED LEG REA VARIABLE LOAD- MAKE UP PRELOA MINIMUM PRELO	C.G.) / CTION CTION STORM MOVE D D D CULATED CULATED CULATED	142.00° 4,053.890 (3,969.098) 84.792 8,650.000 84.792 8,734.792	KIPS KIPS KIPS KIPS KIPS KIPS KIPS	6,582.84 6,691.27 6,670.37 ANGLE OBSERVED TRIM HEEL	BOW RE STBD RE PORT RE 0.10 0.00	ACTION ACTION ACTION DEGRE DEGRE
88 89 90 92 93 94 95 96 97 98 99 200 201 202 203	REACTION BOW LE REACTION STBD LE REACTION PORT LE TOTAL CALCULATEL LESS HOOK, ROTORY LESS CONDUCTOR 1 LESS TOTAL LIGHT TOTAL VARIABLE MAX. VARIABLE LO	G G G G G G G G G G G G G G G G G G G	TOTAL REAC REAC REAC REAC RM) LING) SS RS	L LOADING (- TION ON AFT TION OF AFT) REACTIC LEGS X (7 (-) PORT (-) (+)	ON ON AFT LEGS 71.00' (+) RIG T OR STED LEG REA VARIABLE LOAD- VARIABLE LOAD- MAKE UP PRELOA MINIMUM PRELOA MIN. REQUIRED EST REACTION CAL ALLOWABLE LEG R WIND DIRECTION MAX. WATER DEF	C.C.G.) / CTION STORM MOVE DD DD PRELOAD CULATED REACTION	142.00° 4,053.890 (3,969.098) 84.792 8,650.000 84.792 8,734.792	KIPS KIPS KIPS KIPS KIPS KIPS	6,582.84 6,691.27 6,670.37 ANGLE OBSERVED TRIM HEEL	BOW RE STBD RE PORT RE 0.10 0.00	ACTION ACTION ACTION DEGRE DEGRE
88 89 90 92 93 94 95 96 97 98 99 00 01 02 03 04 05 06	REACTION BOW LE REACTION STBD LE REACTION PORT LE REACTIO	G G G G G G G G G G G G G G G G G G G	TOTAL REAC REAC REAC REAC RM) LING) S S S S S S S S S S S S S S S S S S S	L LOADING (- TION ON AFT TION OF AFT) REACTIC LEGS X (7 (-) PORT (-) (+)	ON ON AFT LEGS 71.00' (+) RIG T OR STED LEG REA VARIABLE LOAD- VARIABLE LOAD- MAKE UP PRELOA MINIMUM PRELOA MAKE UP PRELOA MIN. REQUIRED EST REACTION CAL ALLOWABLE LEG R	C.C.G.) / CTION STORM MOVE DD DD PRELOAD CULATED REACTION	142.00° 4,053.890 (3,969.098) 84.792 8,650.000 84.792 8,734.792	KIPS KIPS KIPS KIPS KIPS KIPS KIPS	6,582.84 6,691.27 6,670.37 ANGLE OBSERVED TRIM HEEL	BOW RE STBD RE PORT RE 0.10 0.00	ACTION ACTION ACTION DEGRE DEGRE
88 89 90 92 93 94 95 96 97 98 99 00 01 02 33 04 05 06 07 08	REACTION BOW LE REACTION STBD LE REACTION PORT LE LESS HOOK, ROTORY LESS TOTAL LIGHT TOTAL VARIABLE LO MAX. VARIABLE LO MAX. VARIABLE LO MAX. VARIABLE LO ROTABLE WATER TO """" DRILL WATER TO	G G G G G G G G G G G G G G G G G G G	TOTAL REAC'	L LOADING (- TION ON AFT TION OF AFT) REACTIC LEGS X (7 (-) PORT (-) (+)	ON ON AFT LEGS 71.00' (+) RIG T OR STED LEG REA VARIABLE LOAD- VARIABLE LOAD- MAKE UP PRELOA MINIMUM PRELOA MIN. REQUIRED EST REACTION CAL ALLOWABLE LEG R WIND DIRECTION MAX. WATER DEF	C.C.G.) / CTION STORM MOVE D D PRELOAD CULATED REACTION	142.00° 4,053.890 (3,969.098) 84.792 8,650.000 84.792 8,734.792	KIPS KIPS KIPS KIPS KIPS KIPS KIPS	6,582.84 6,691.27 6,670.37 ANGLE OBSERVED TRIM HEEL	BOW RE STBD RE PORT RE 0.10 0.00	ACTION ACTION ACTION DEGRE DEGRE
88 89 90 92 93 94 95 96 97 98 99 90 00 01 02 03 04 05 06 07	REACTION BOW LE REACTION STBD LE REACTION PORT LE REACTIO	G G G G G G G G G G G G G G G G G G G	TOTAL REAC'	L LOADING (- TION ON AFT TION OF AFT) REACTIC LEGS X (7 (-) PORT (-) (+)	ON ON AFT LEGS 71.00' (+) RIG TOOR STED LEG REA VARIABLE LOAD- VARIABLE LOAD- MAKE UP PRELOA MINIMUM PRELOA MIN. REQUIRED EST REACTION CAL ALLOWABLE LEG R WIND DIRECTION MAX. WATER DEF MAX. WINDS SPE	C.C.G.) / CTION STORM MOVE D D PRELOAD CULATED REACTION	142.00° 4,053.890 (3,969.098) 84.792 8,650.000 84.792 8,734.792	KIPS KIPS KIPS KIPS KIPS KIPS KIPS KIPS	6,582.84 6,691.27 6,670.37 ANGLE OBSERVED TRIM HEEL	BOW RE STBD RE PORT RE 0.10 0.00	ACTION ACTION ACTION CACTION C
88 89 90 92 93 94 95 96 97 98 99 00 01 02 03 04 05 06 07 08	REACTION BOW LE REACTION STBD LE REACTION PORT LE REACTIO	G G G G G G G G G G G G G G G G G G G	TOTAL REAC'	L LOADING (- TION ON AFT TION OF AFT) REACTIC LEGS X (7 (-) PORT (-) (+)	ON ON AFT LEGS 71.00' (+) RIG TOOR STED LEG REA VARIABLE LOAD- VARIABLE LOAD- MAKE UP PRELOA MINIMUM PRELOA MIN. REQUIRED EST REACTION CAL ALLOWABLE LEG R WIND DIRECTION MAX. WATER DEF MAX. WINDS SPE	C.C.G.) / CTION STORM MOVE D D PRELOAD CULATED REACTION	142.00° 4,053.890 (3,969.098) 84.792 8,650.000 84.792 8,734.792	KIPS KIPS KIPS KIPS KIPS KIPS KIPS KIPS	6,582.84 6,691.27 6,670.37 ANGLE OBSERVED TRIM HEEL	BOW RE STBD RE PORT RE 0.10 0.00	ACTION ACTION ACTION CACTION C
88 89 90 92 93 94 95 96 97 98 99 00 01 02 3 04 05 06 07 08 09 10	REACTION BOW LE REACTION STBD LE REACTION PORT LE REACTIO	G G G G G G G G G G G G G G G G G G G	TOTAL REAC'S REA	L LOADING (- TION ON AFT TION OF AFT 19,944.478 0.000 0.000 (15,975.380) 3,969.098 4,053.890 5,553.890 4,009.490 1,491.46 62,641.52 233.28 237,098.14 2,140.76 89,912 550.45 340,317 3,752.84) REACTIC LEGS X (7 (-) PORT (-) (+)	ON ON AFT LEGS 71.00' (+) RIG TOOR STED LEG REA VARIABLE LOAD- VARIABLE LOAD- MAKE UP PRELOA MINIMUM PRELOA MIN. REQUIRED EST REACTION CAL ALLOWABLE LEG R WIND DIRECTION MAX. WATER DEF MAX. WINDS SPE	C.C.G.) / CTION STORM MOVE D D PRELOAD CULATED REACTION	142.00° 4,053.890 (3,969.098) 84.792 8,650.000 84.792 8,734.792	KIPS KIPS KIPS KIPS KIPS KIPS KIPS KIPS	6,582.84 6,691.27 6,670.37 ANGLE OBSERVED TRIM HEEL	BOW RE STBD RE PORT RE 0.10 0.00	ACTION ACTION ACTION CONTROL DEGRI DEGRI FEET

		TRANSIT CONDITION =	FIELD TRANSIT	DATE:	NOV 1,1990
10.		WIND VELOCITY = 70 Kts.	CALCULATED BY:	SHEET:	1 OF 2
**==	No.	:=====================================	SOURCE	TOTAL	UNITS
327	PARTI	CULARS			
328	A	DISPLACEMENT	FROM LOAD FORM ITEM 152	19,944.48	KIPS
329	В	DRAFT	FROM HYDROSTATICS	14.35	FEET
330	C	KG, UNCORRECTED	FROM LOAD FORM ITEM 152	54.88	FEET
331	D	CALCULATED FSC DISPLACEMENT	CHAPTER 4 SECTION 3	19,040.00	KIPS
332	Ē	LFSC SUM	FROM LOAD FORM ITEM 152	0.9174	FEET
333	F	CORRECTED LFSC	[F]=([E]X[D])/[A]	0.8758	FEET
334	Ġ	TFSC SUM	FROM LOAD FORM ITEM 152	0.8455	FEET
335	H	CORRECTED TESC	[H]=([G]X[D])/[A]	0.8072	FEET
336	•	EXPOSEST ESC CORRECTED	MAXIMUM [F] OR [H]	0.8758	FEET
550	====	=======================================		==========	
338	STAB	ILITY CALCULATION	F 17 - F03 + F13	55.76	FEET
339	J	CORRECTED KG	[J]=[C]+[I]	80.27	FEET
340	K	ALLOWABLE KG	ALLOWABLE KG CURVES		
7/2		AND HEEL CALCULATIONS			
342 343	L	HULL LENGTH	FROM CHAPTER 1, SECTION 4	247.58	FEET
	M	HULL WIDTH	FROM CHAPTER 1, SECTION 4	200.50	FEET
344		KWL @ [B]	FROM HYDROSTATICS	209.09	FEET
345	N	CORRECTED KGL	[P] = [C] + [F]	55.76	FEET
346	P	GML	[Q] = [N] - [P]	153.34	FEET
347	Q		[R]=([Q]X[A])/HULL LENGTH	12,352.35	FT. KIPS
348	R	MT1' @ [B]	FROM HYDROSTATICS	141.10	FEET
349	S	LCB @ [B]	FROM LOAD FORM ITEM 152	141.42	FEET
350	Ť	LCG TRIMMING LEVER (LCG-LCB)	[U] = [T] - [S]	0.32	FEET
351	U		[V] = [A] X [U] / [R]	0.52	FEET
352	٧	TRIM (FT.)	[W] = ([U] X57.3)/[Q]	0.12	DEGREES
353	W	TRIM (DEG)	FROM HYDROSTATICS	140.23	FEET
354	X	KWI 9 [B]	[Y] = [C] + [H]	55.69	FEET
355	Y	CORRECTED KGT	[Z] = [X] - [Y]	84.54	FT. KIPS
356	Z	GMT	[AA]=([Z]X[A])/HULL WIDTH	8,409.99	FT. KIPS
357	AA	MH1' @ [B]	FROM LOAD FORM ITEM 152	0.11	FEET
358	BB	TCG	[CC]=([.074-[BB])*[A]/[AA]	0.09	FEET
359	CC	HEEL (FEET)	[DD]=([BB]/[Z]*57.3)	0.06	DEGREES
360	DD	HEEL (DEG)	DRAFT MARK PORT HULL	1.00	
361	EE	DRAFT BOW PORT HULL-LCG	DRAFT MARK PORT HULL	(5.00) FEET
362		DRAFT BOW PORT HULL-TCG	DRAFT MARK KEY SLOT	208.00	
363		DRAFT KEY SLOT-LCG	DRAFT MARK KEY SLOT	26.00	
364		DRAFT KEY SLOT-TCG	DRAFT MARK PORT HULL	196.00	
365		DRAFT PORT HULL-LCG	DRAFT MARK PORT HULL	(98.00	
366		DRAFT PORT HULL-TCG	DRAFT MARK STBD HULL	196.00	
367		DRAFT STBD. HULL-LCG	DRAFT MARK STED HULL	98.00	
368		DRAFT STBD HULL-TCG	FROM HYDROSTATICS	144.22	
369		LCF a[A]	DRAFT=[B] - [V]X([NN] - [EE])/[L]+[CC]([FF]/[M]	14.05	
370		DRAFT BOW PORT HULL	DBV21-103-103A(1003-1003/113-1003/1001/1003/1003/1003/1	14.47	
371		DRAFT KEY SLOT	DRAFT=[B] - [V] X([NN] - [GG]) / [L] - [CC] ([HH] / [M]	14.41	
372	RR	DRAFT PORT HULL	DRAFT=[B]+[V]X([JJ]-[NN])/[L]+[CC]([KK]/[M]	14.50	
373	SS	DRAFT STBD HULL	DRAFT=[B]+[V]X([LL]-[NN])/[L]+[CC]([MM]/[M] 		

1 5 JOE 1991

ITEM NO.	RIG:	TRANSIT CONDITION = WIND VELOCITY = 100 Kts.	LONG MOVES CALCULATED BY:	DATE:	NOV 1,19
		T.O.C. DOWN 45.90 FT.		, SHEET:	2 OF
	No.	ITEM	SOURCE	TOTAL	UNITS
395	PARTI	CULARS			
396	A	DISPLACEMENT	FROM LOAD FORM ITEM 155	19,944.48	KIPS
397	В	DRAFT	FROM HYDROSTATICS	14.35	FEET
398	С	KG, UNCORRECTED	FROM LOAD FORM ITEM 155	45.19	FEET
399	D	CALCULATED FSC DISPLACEMENT	CHAPTER 4 SECTION 3	19,040.00	KIPS
400	E	LFSC SUM	FROM LOAD FORM ITEM 155	0.9174	FEET
401	F	CORRECTED LFSC	[F]=([E]X[D])/[A]	0.8758	FEET
402	G	TFSC SUM	FROM LOAD FORM ITEM 155	0.8455	FEET
403	н	CORRECTED TFSC	[H]=([G]X[D])/[A]	0.8072	FEET
404	1	LARGEST FSC, CORRECTED	MAXIMUM [F] OR [H]	0.8758	FEET
	=====	•			
406		LITY CALCULATION			
407	J	CORRECTED KG	[J]=[C]+[I]	46.07	FEET
408	K	ALLOWABLE KG	ALLOWABLE KG CURVES	58.61	FEET
	=====			============	
410	TRIM	AND HEEL CALCULATIONS			
411	L	HULL LENGTH	FROM CHAPTER 1, SECTION 4	243.08	FEET
412	M	HULL WIDTH	FROM CHAPTER 1, SECTION 4	200.50	FEET
413	N	KML a [B]	FROM HYDROSTATICS	209.09	FEET
414	P	CORRECTED KGL	[P] = [C] + [F]	46.07	FEET
415	Q	GML	[Q] = [N] - [P]	163.02	FEET
416	R	MT1' @ [B]	[R]=([Q]X[A])/HULL LENGTH	13,376.02	FT. KIF
417	S	LCB @ [B]	FROM HYDROSTATICS	141.10	FEET
418	T	LCG	FROM LOAD FORM ITEM 155	141.42	FEET
419	U	TRIMMING LEVER (LCG-LCB)	[U] = [T] - [S]	0.32	FEET
420	٧	TRIM (FT.)	[V] = [A] X [U] / [R]	0.48	FEET
421	W	TRIM (DEG)	[W]=([U]X57.3)/[Q]	0.11	DEGREE
422	X	KMT @ [B]	FROM HYDROSTATICS	140.23	FEET
423	Y	CORRECTED KGT	[Y] = [C] + [H]	46.00	FEET
424	Z	GMT	(Z) = (X) - (Y)	94.23	FT. KIP
425	AA	MH1' a [B]	[AA]=([Z]X[A])/HULL WIDTH	9,373.82	FT. KIP
426	BB	TCG	FROM LOAD FORM ITEM 155	0.11	FEET
427	CC	HEEL (FEET)	[CC] = ([.074 - [BB]) * [A] / [AA]	0.08	FEET
428	DD	HEEL (DEG)	[DD]=([BB]/[Z]*57.3)	0.05	DEGREE
429	EE	DRAFT BOW PORT HULL-LCG	DRAFT MARK PORT HULL	1.00	FEET
430	FF	DRAFT BOW PORT HULL-TCG	DRAFT MARK PORT HULL	(5.00)	FEET
431	GG	DRAFT KEY SLOT-LCG	DRAFT MARK KEY SLOT	208.00	FEET
432	HH	DRAFT KEY SLOT-TCG	DRAFT MARK KEY SLOT	26.00	FEET
433	JJ	DRAFT PORT HULL-LCG	DRAFT MARK PORT HULL	196.00	FEET
434	KK	DRAFT PORT HULL-TCG	DRAFT MARK PORT HULL	(98.00)	FEET
435	LL	DRAFT STBD. HULL-LCG	DRAFT MARK STBD HULL	196.00	FEET
436	ММ	DRAFT STBD HULL-TCG	DRAFT MARK STBD HULL	98.00	FEET
437	NN	LCF a[A]	FROM HYDROSTATICS	144.22	FEET
438	PP	DRAFT BOW PORT HULL	DRAFT=[B] - [V] X([NN] - [EE])/[L] + [CC] ([FF] / [M]	14.06	FEET
439	00	DRAFT KEY SLOT	DRAFT=[B] - [V] X([NN] - [GG])/[L] - [CC] ([HH]/[M]	14.46	FEET
440	RR	DRAFT PORT HULL	DRAFT=[B]+[V]X([JJ]-[NN])/[L]+[CC]([KK]/[M]	14.41	FEET
				17.71	

ADDENDUM B FEBRUARY 13, 1991

