



## IMCO

### INTERNATIONAL CONFERENCE ON TONNAGE MEASUREMENT, 1969

#### Technical Committee

#### PROGRESS REPORT OF THE WORKING GROUP ON GROSS AND NET TONNAGE (Part II)

8. On 9 and 10 June 1969 the Working Group under the Chairmanship of Mr. P. Eriksson (Sweden) attended by its members as listed in paragraph 1 of Part I of the progress report (TM/CONF/C.2/WP.19) continued with its work after having received further results of the computer calculations.

$$\underline{\text{Formula NT} = a_1 \nabla}$$

9. In addition to the computer exercises reported in paragraph 7(b) the following studies have been carried out:

(a) Out of the IMCO fleet all those ships were selected for which no deduction for water ballast spaces in the tonnage certificate were shown. This selection comprised mainly small ships. The results of the exercises are shown at Annex III column 1.

(b) For the logarithmic type of the formula in addition to the exercises reported in paragraph 7(b) the following coefficients were tested:

$$A = 0.1 + 0.05 \log_{10} \nabla \quad \text{and}$$

$$A = 0.125 + 0.04 \log_{10} \nabla$$

the results being shown at Annex III columns 2 and 3.

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$$\text{Formula NT} = a_1 \nabla + a_2 \text{"P} - a_3 \text{"WB}$$

10. The above formula was investigated by Group III.

(a) However as the data of the IMCO fleet did not include the total volume of ballast water spaces but were only available for a restricted number of mainly British and Japanese ships, a computer exercise for this formula was not possible. The formula without the second term in the form  $\text{NT} = 0.29\nabla - 0.21\text{WB}$  and in the form  $\text{NT} = A(\nabla - \text{WB})$  were investigated.

The computer exercise was carried out using the water ballast deduction of the IMCO and UK data corrected to total amount of water ballast using the ratio between total and deducted amount calculated for certain Japanese and British ships. In the exercise passenger ships were excluded.

The results of the computer exercises for the above two formulae are shown at Annex IV.

(b) As, however, for instance for ore carriers the amount of water ballast can be of the order of 60 - 80 per cent of the displacement, it was agreed that a lower limit of net tonnage was needed. For this limit  $\text{NT} > 0.3 \text{ GT}$  was proposed.

(c) Regarding the passenger term  $a_2 \text{"P}$  of the formula above the expression  $P = N_b + \frac{N_u}{10}$  was used resulting from studies by Denmark and Italy and for the coefficient  $a_2 \text{"} = 1 + \frac{\nabla}{10,000}$  was suggested tentatively.

The results of the computer study using the formula  $\text{NT} = 0.29\nabla + (1 + \frac{\nabla}{10,000})(N_b + \frac{N_u}{10})$  for the passenger ships of the IMCO fleet are shown at Annex V.

11. Having accomplished the computer studies mentioned under paragraph 10(a) the Working Group decided to repeat the calculation for two groups of ships below and above 2,000 GT in order to

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cover more comprehensively the size of ships. The results of this additional study for the second formula are given at Annex VI.

General remarks

12. At the request of the Danish delegation its paper TM/CONF/C.2/WP.10 and TM/CONF/C.2/WP.10/Add.1 were considered. However, in view of the decision by the Technical Committee that the gross tonnage should not be function of displacement, draught or freeboard, only a brief discussion took place and no decision was taken.

ANNEX III

| Formula                      | $NT = AV$    | $NT = V(A+B \log_{10} V)$ |                            |
|------------------------------|--------------|---------------------------|----------------------------|
| Coefficients                 | $A = 0.2461$ | $A = 0.1$<br>$B = 0.05$   | $A = 0.125$<br>$B = 0.047$ |
| Total No. of Ships           | 47           | 591                       | 591                        |
| No. of ships retained        | 46           | 561                       | 560                        |
| Percentage of mean deviation | 8,057        | -7.917                    | -12.338                    |
| $SD_o$                       | 28.699       | 24.553                    | 27.338                     |
| $SD_m$                       | 27.519       | 23.5239                   | 24.195                     |
| Fleet per cent change        | 24.028       | -4.422                    | -8.514                     |

ANNEX IV

| Formula                      | $NT = AV - B(WB)$         | $NT = A(\nabla - WB)$ |
|------------------------------|---------------------------|-----------------------|
| Coefficient                  | $A = 0.29 \quad B = 0.21$ | $A = 0.2953$          |
| Total No. of ships           | 516                       | 516                   |
| No. of ships retained        | 486                       | 482                   |
| Percentage of mean deviation | 1.651                     | 3.429                 |
| $SD_o$                       | 16.701                    | 18.536                |
| $SD_m$                       | 16.619                    | 18.216                |
| Fleet change                 | 9.882                     | 12.099                |

ANNEX V

$$NT = .29 \nabla + (1 + \frac{\nabla}{10,000})(N_b + \frac{N_u}{10})$$

Results:

Percentage of Mean Dev.    -15.7320  
                               SD<sub>o</sub>                29.296  
                               SD<sub>M</sub>                24.6644  
 Fleet per cent change       -17.92

| <u>Name</u> | <u>R.N.T.</u> | <u>F.N.T.</u> | <u>Percentage<br/>Deviation</u> |
|-------------|---------------|---------------|---------------------------------|
| LP-1        | 2616          | 1263.77       | -51.69                          |
| LP-2        | 1318          | 1079.19       | -18.11                          |
| NP-34       | 11489         | 8579.04       | -25.32                          |
| -35         | 2600          | 1899.97       | -26.92                          |
| -36         | 2562          | 1899.97       | -25.84                          |
| -37         | 3488          | 2489.03       | -28.64                          |
| -38         | 3522          | 2390.69       | -32.12                          |
| SP-34       | 12883         | 11047.79      | -14.24                          |
| KP-43       | 13900         | 9089.05       | -34.61                          |
| -44         | 21880         | 14815.36      | -32.28                          |
| -45         | 11625         | 9645.00       | -17.03                          |
| UP-1        | 2061          | 2114.11       | 2.57                            |
| -2          | 1322          | 1164.93       | -11.88                          |
| GP-1        | 15694         | 13277.20      | -15.39                          |
| -2          | 12167         | 10330.00      | -15.09                          |
| -3          | 17227         | 15587.50      | -9.510                          |
| -4          | 24572         | 21340.30      | -13.15                          |
| -5          | 6633          | 4416.23       | -33.42                          |
| -6          | 15962         | 14161.56      | -10.15                          |

| <u>Name</u> | <u>R.N.T.</u> | <u>F.N.T.</u> | <u>Percentage<br/>Deviation</u> |
|-------------|---------------|---------------|---------------------------------|
| QP-1        | 519           | 451.24        | -13.05                          |
| -2          | 1379          | 811.51        | -41.15                          |
| -3          | 1608          | 947.00        | -41.10                          |
| YP-27       | 13536         | 15312.88      | 13.12                           |
| -28         | 11229         | 12756.48      | 13.60                           |
| FP-1        | 36063         | 29829.28      | -17.28                          |
| -2          | 7739          | 4982.34       | -35.62                          |
| KM-46       | 2868          | 2505.58       | -12.63                          |
| -47         | 3793          | 2336.63       | -38.39                          |
| -48         | 4707          | 4260.63       | -9.48                           |
| GM-1        | 3624          | 2741.26       | -24.35                          |
| -2          | 2758          | 2218.60       | -19.55                          |
| -3          | 6406          | 5938.07       | -7.30                           |
| -4          | 2990          | 2210.86       | -26.05                          |
| -5          | 2311          | 1699.94       | -26.44                          |
| -6          | 2495          | 1752.32       | -29.76                          |
| -7          | 7240          | 5779.00       | -20.17                          |
| QM-1        | 814           | 558.66        | -31.36                          |
| -2          | 1167          | 914.13        | -21.66                          |
| -3          | 320           | 270.25        | -15.54                          |
| -4          | 7272          | 6399.74       | -11.99                          |
| OM-1        | 5418          | 4797.91       | -11.44                          |
| -2          | 773           | 695.58        | -10.01                          |
| SM-36       | 20928         | 15985.10      | -23.61                          |
| YM-29       | 7496          | 6895.00       | -8.01                           |
| -30         | 4327          | 4203.12       | -2.86                           |
| -31         | 4916          | 4332.40       | -11.87                          |
| FM-1        | 7263          | 5810.20       | -20.00                          |
| -2          | 7194          | 5918.24       | -17.73                          |
| -3          | 7022          | 5193.79       | -26.03                          |

| <u>Name</u> | <u>R.N.T.</u> | <u>F.N.T.</u> | <u>Percentage<br/>Deviation</u> |
|-------------|---------------|---------------|---------------------------------|
| AZ-1        | 2355          | 2031.85       | -13.72                          |
| -2          | 1480          | 1283.07       | -13.30                          |
| LZ-1        | 1195          | 1071.42       | -10.34                          |
| -2          | 467           | 539.47        | 15.51                           |
| NZ-41       | 1096          | 1004.66       | -8.33                           |
| -42         | 933           | 851.17        | -8.77                           |
| -43         | 352           | 454.27        | 29.05                           |
| -44         | 744           | 616.84        | -17.09                          |
| SZ-37       | 1335          | 1328.12       | -0.51                           |
| FZ-1        | 2914          | 1798.40       | -38.28                          |
| KZ-50       | 2825          | 1052.80       | -62.73                          |
| GZ-1        | 687           | 608.53        | -11.42                          |
| -2          | 1013          | 1748.89       | 72.64                           |
| -3          | 2006          | 1773.85       | -11.57                          |
| -4          | 2572          | 1608.32       | -37.46                          |
| -5          | 2691          | 2421.72       | -10.00                          |
| W-1         | 528           | 665.14        | 25.97                           |
| -2          | 2880          | 1845.55       | -35.91                          |
| -3          | 4298          | 2033.71       | -52.68                          |
| OZ-1        | 1759          | 2216.00       | 25.98                           |
| -2          | 1532          | 1263.23       | -17.54                          |
| SA-35       | 3276          | 2340.30       | -28.56                          |
| NX-39       | 2100          | 1642.29       | -21.79                          |
| -40         | 2791          | 1642.29       | -41.15                          |
| LX-1        | 692           | 1222.00       | 76.58                           |
| -2          | 797           | 1078.42       | 35.30                           |
| KX-49       | 2730          | 1741.60       | -36.20                          |
| GX-1        | 288           | 254.14        | -11.75                          |
| UF-1        | 3521          | 346.48        | -90.15                          |
| -2          | 2868          | 2505.58       | -12.63                          |

ANNEX VI

| Limitation                   | ≤2000 GRT             | >2000 GRT    |
|------------------------------|-----------------------|--------------|
| Formula                      | $NT = A(\nabla - WB)$ |              |
| Coefficient                  | $A = 0.2331$          | $A = 0.3093$ |
| Total No. of Ships           | 111                   | 405          |
| No. of ships retained        | 107                   | 382          |
| Percentage of mean deviation | 5.514                 | 2.545        |
| $SD_n$                       | 23.593                | 15.974       |
| $SD_m$                       | 22.933                | 15.770       |
| Fleet per cent change        | 9.423                 | 8.378        |